

Simulating Complex Power- Ground Plane Shapes with Variable-Size Cell SPICE Grids

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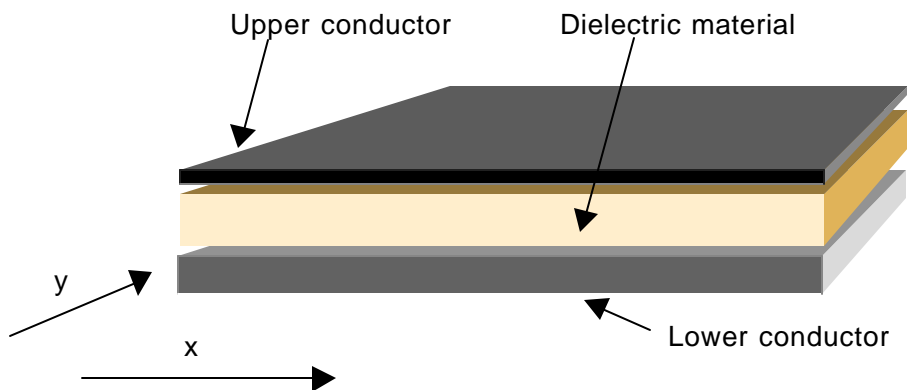
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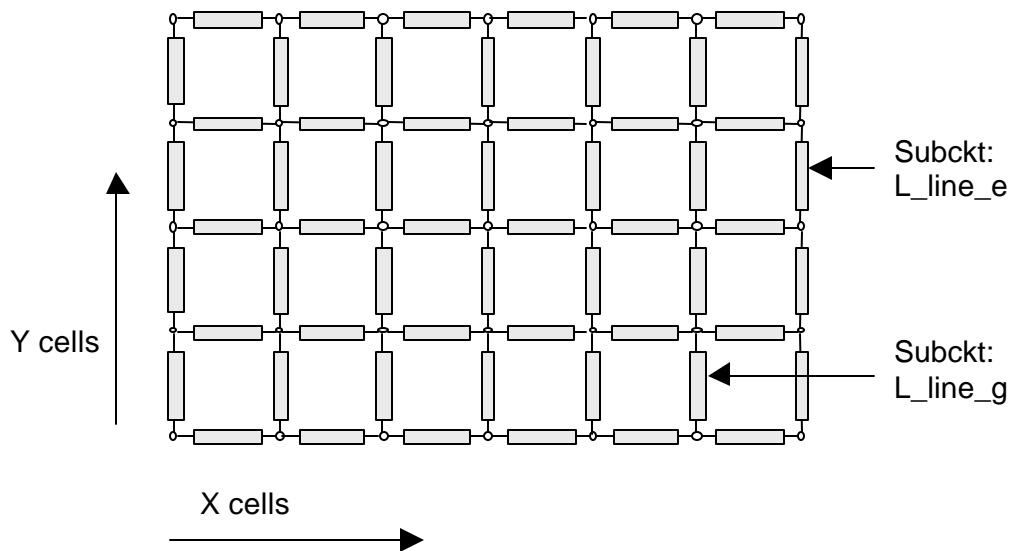
Outline

- Uniform, rectangular plane models
- Need for adaptive, non-uniform grids
- Impedance profiles with various cutouts
- Hardware correlation with adaptive grid
- Conclusions

Conductive plane pair with dielectric separation:



Grid subcircuit model:



Simulation Model for Plane Pairs

(Rectangular and Uniform)

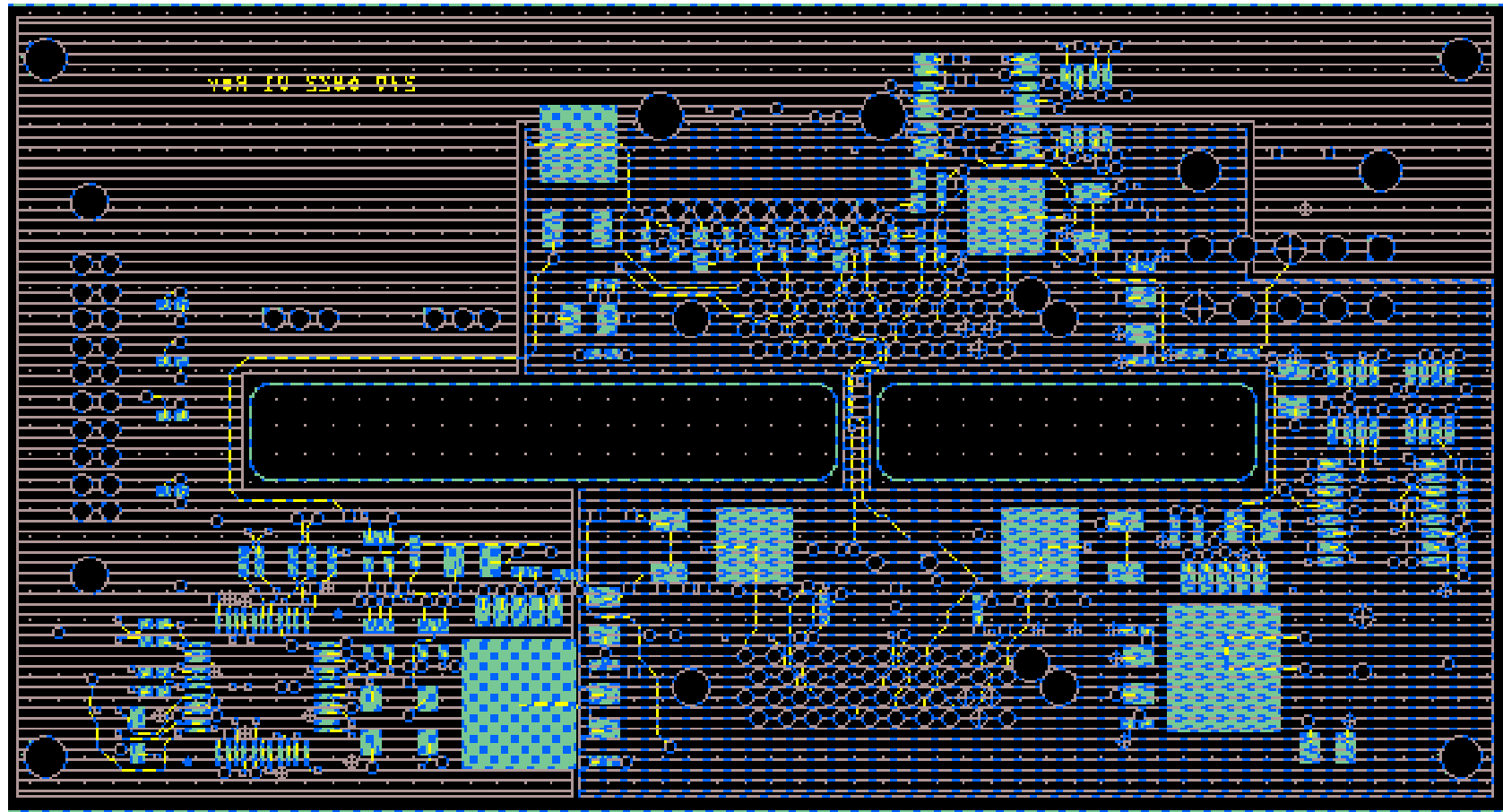
Complex plane shapes

3

EPEP2002

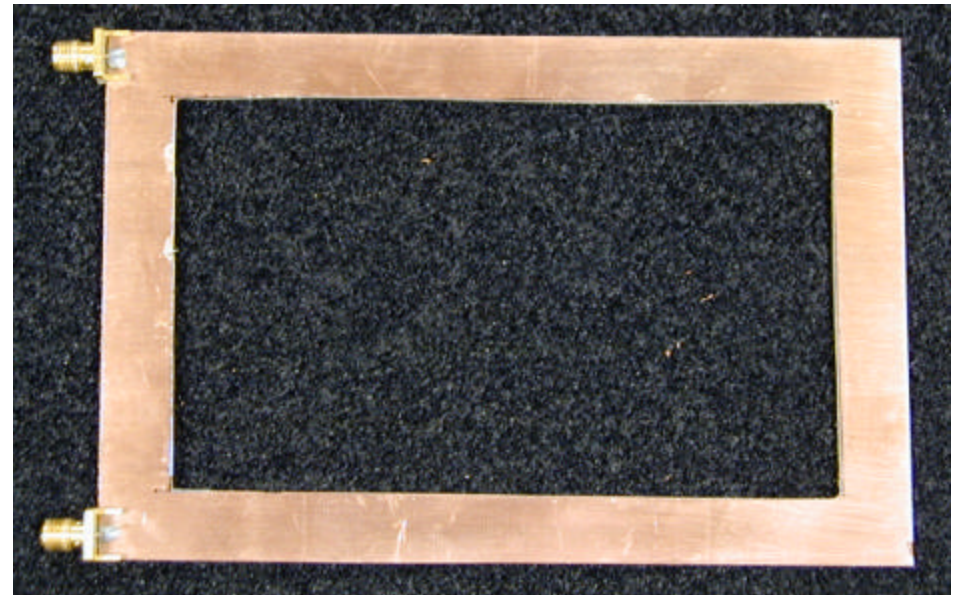


Irregular Plane Shape with Cutouts

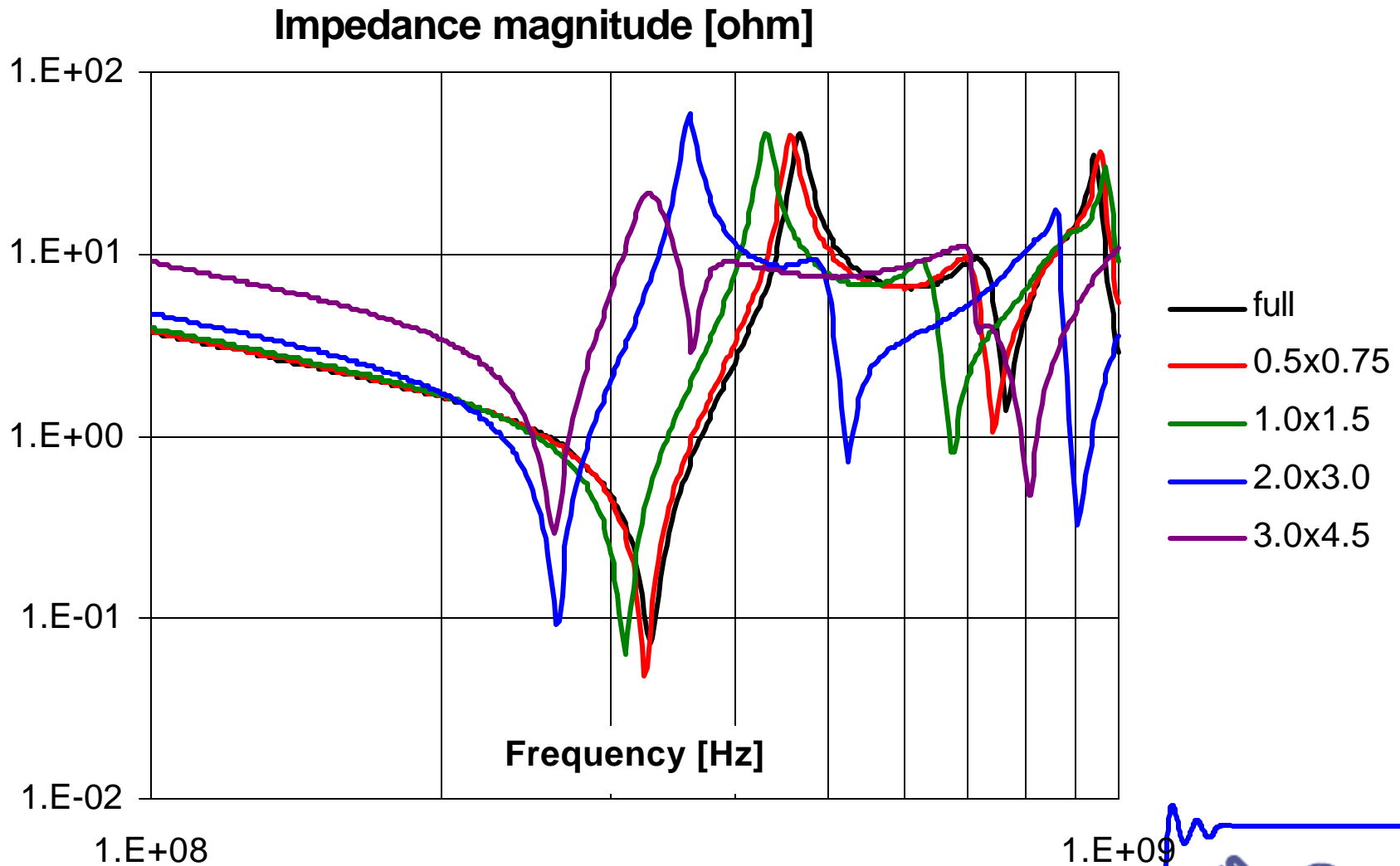


Symmetrical Cutout in Middle (1)

- 1/16" FR4 double-sided 4"x6" rectangular plane pair
- Transfer impedance along shorter side
- Removed copper
 - None
 - 0.5"x0.75" rectangular cutout
 - 1"x1.5" rectangular cutout
 - 2"x3" rectangular cutout
 - 3"x5" rectangular cutout

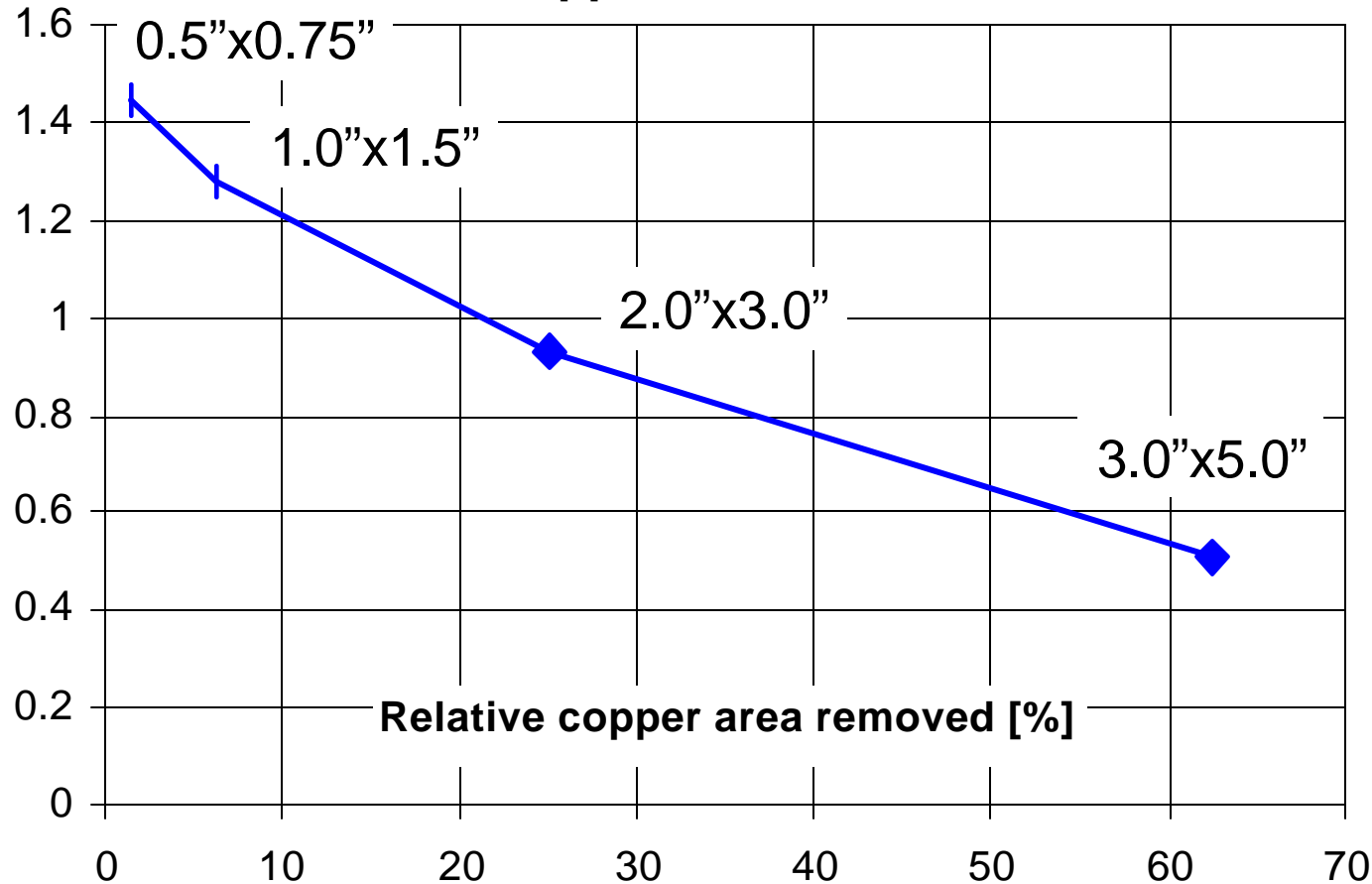


Symmetrical Cutout in Middle (2)



Symmetrical Cutout in Middle (3)

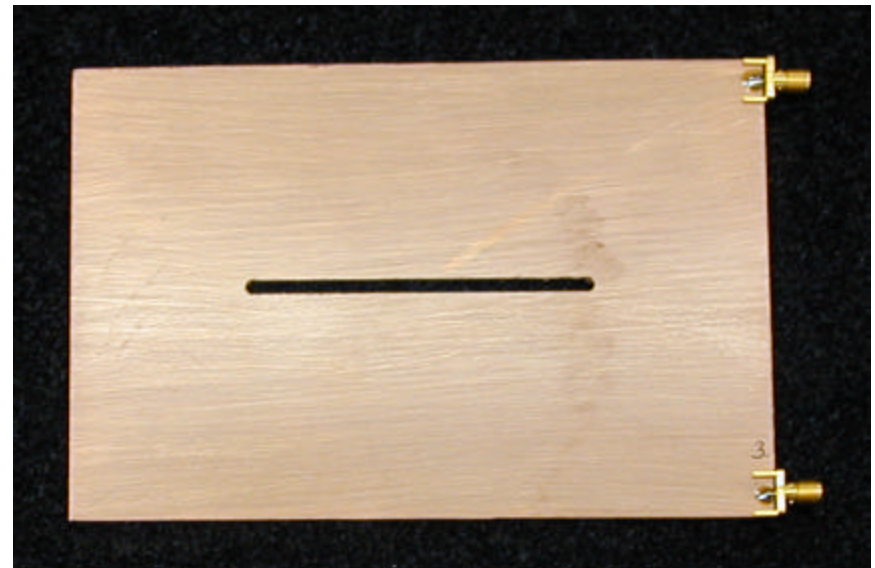
Percentage frequency change over percentage copper removed



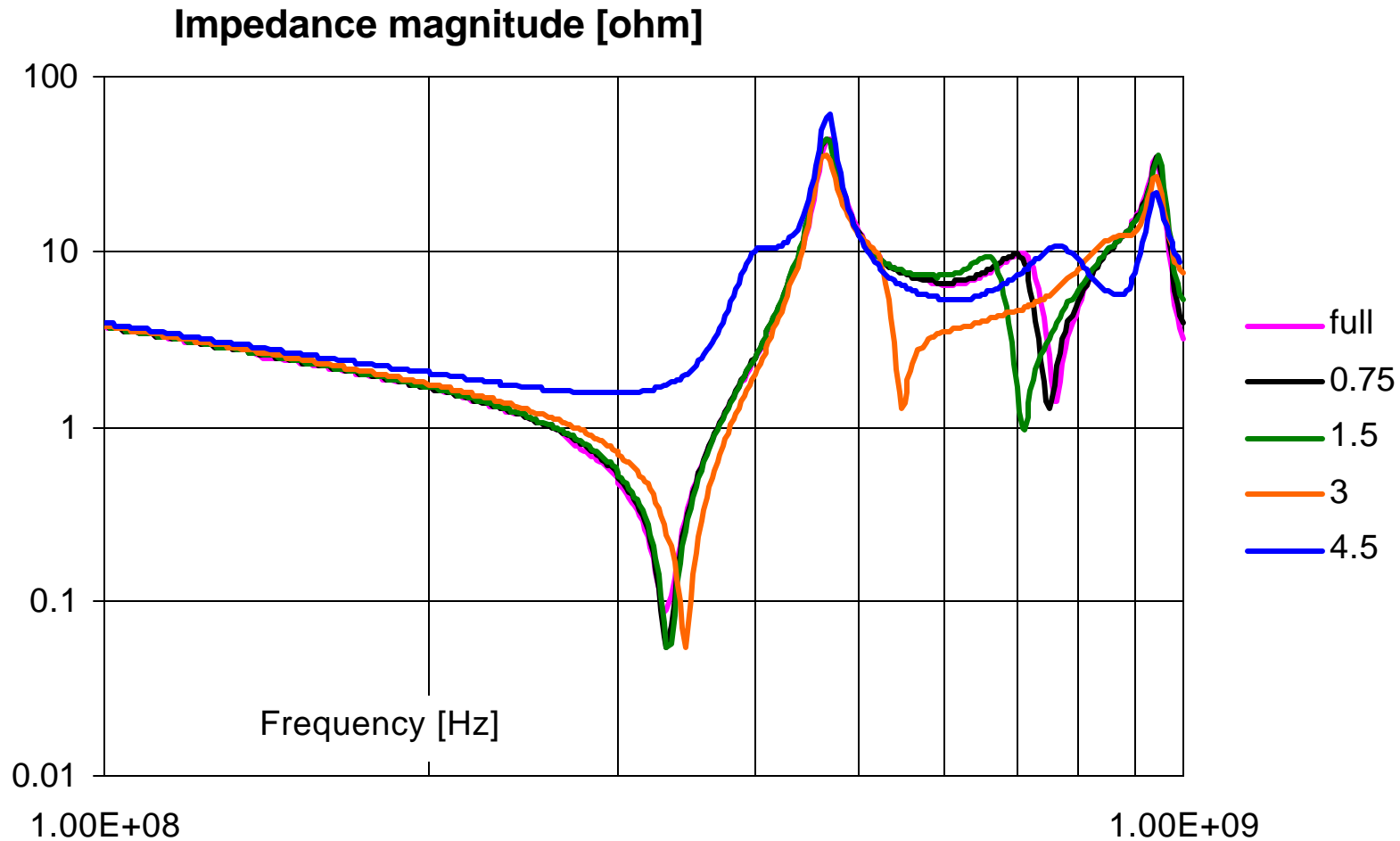
Frequency of first modal resonance peak

Symmetrical Slot in Middle (1)

- 1/16" FR4 double-sided 4"x6" rectangular plane pair
- Transfer impedance along shorter side
- Slot in middle, 0.125" wide
 - None
 - 0.75" rectangular cutout
 - 1.5" rectangular cutout
 - 3" rectangular cutout
 - 4.5" rectangular cutout

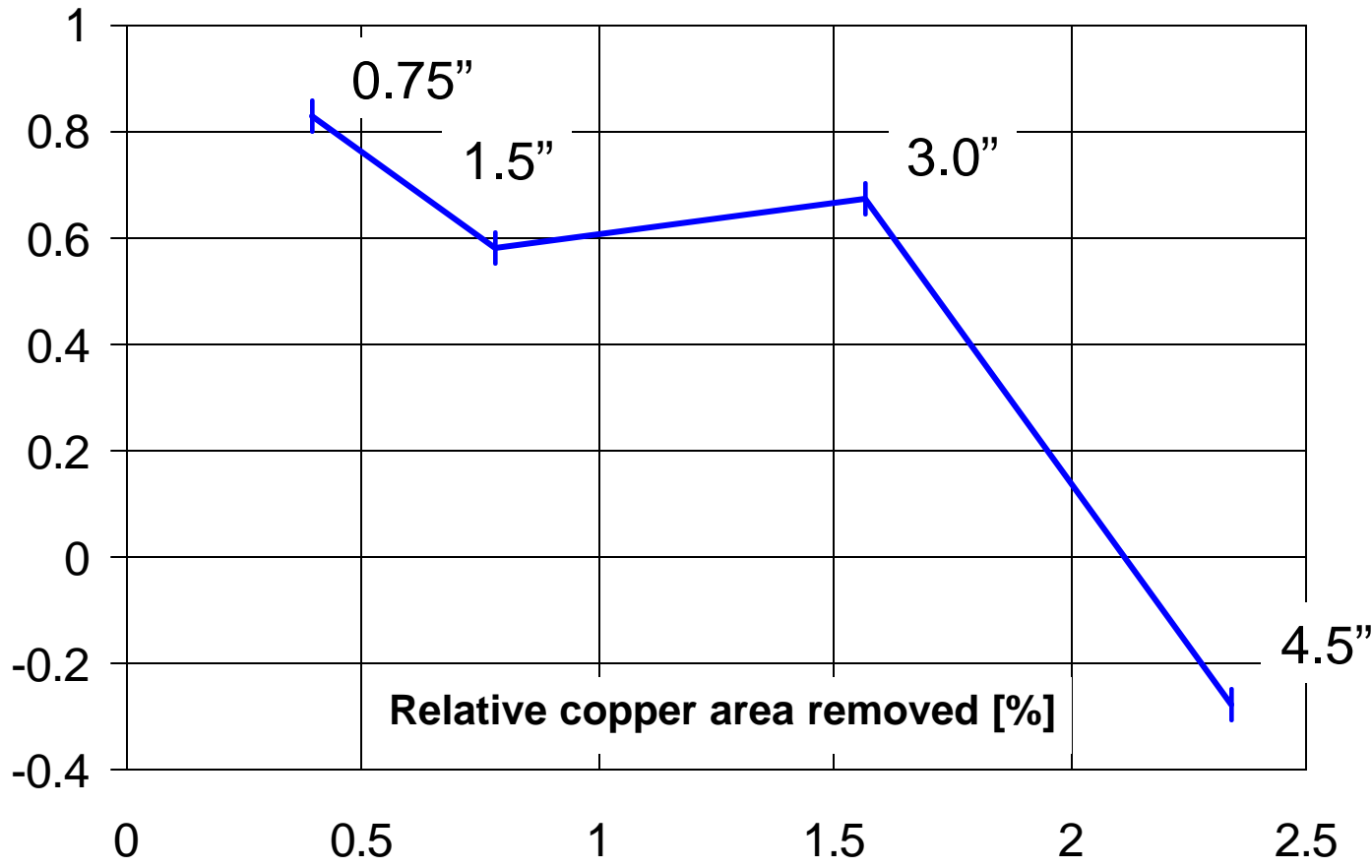


Symmetrical Slot in Middle (2)



Symmetrical Slot in Middle (3)

Percentage frequency change over percentage copper removed



Frequency of first modal resonance peak

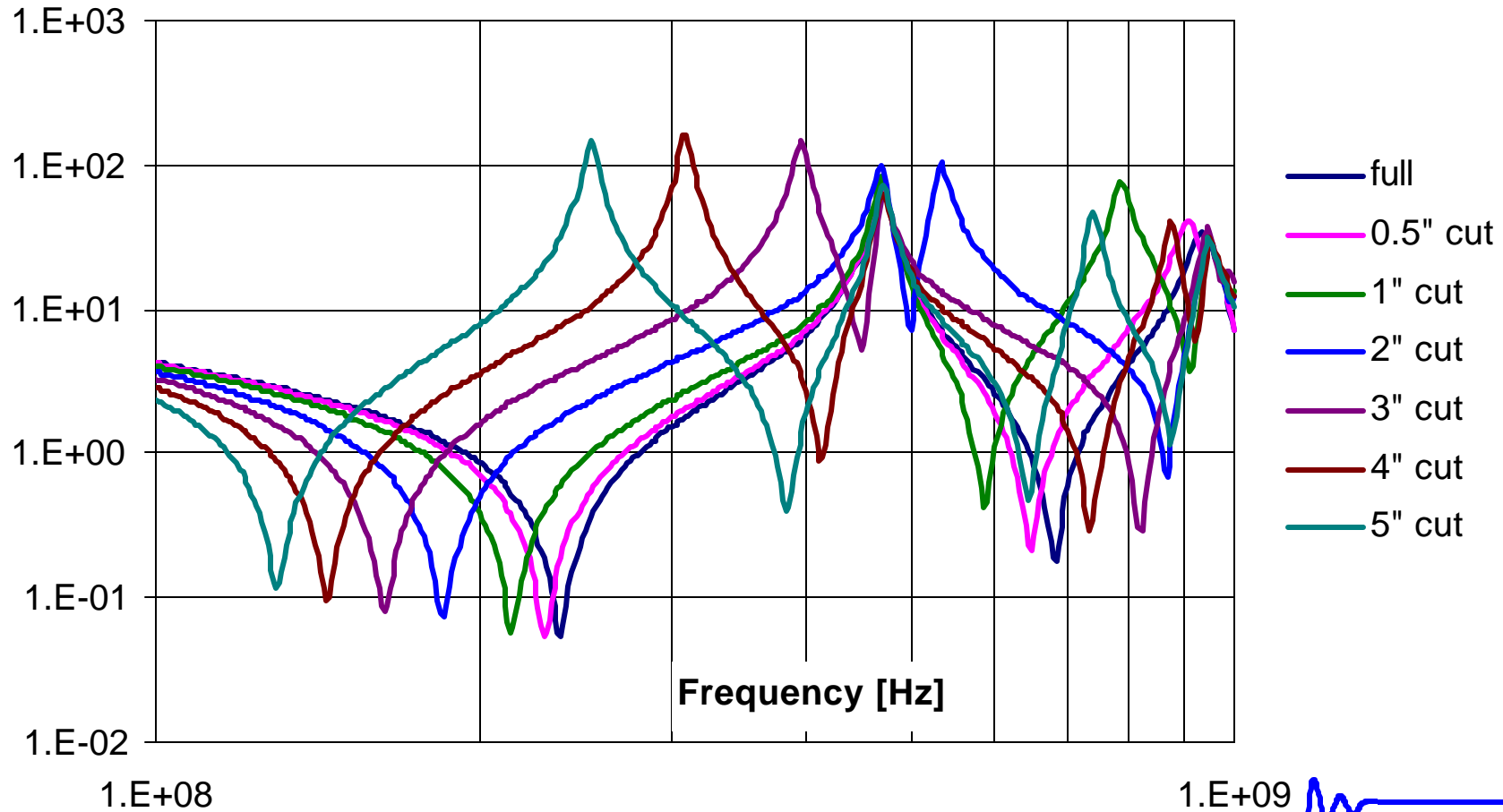
Cut from Side (1)

- 1/16" FR4 double-sided 3"x6" rectangular plane pair
- Transfer impedance along 1" on side
- Cut from side, 0.03" wide
 - None
 - 0.5" cut
 - 1" cut
 - 2" cut
 - 3" cut
 - 4" cut
 - 5" cut



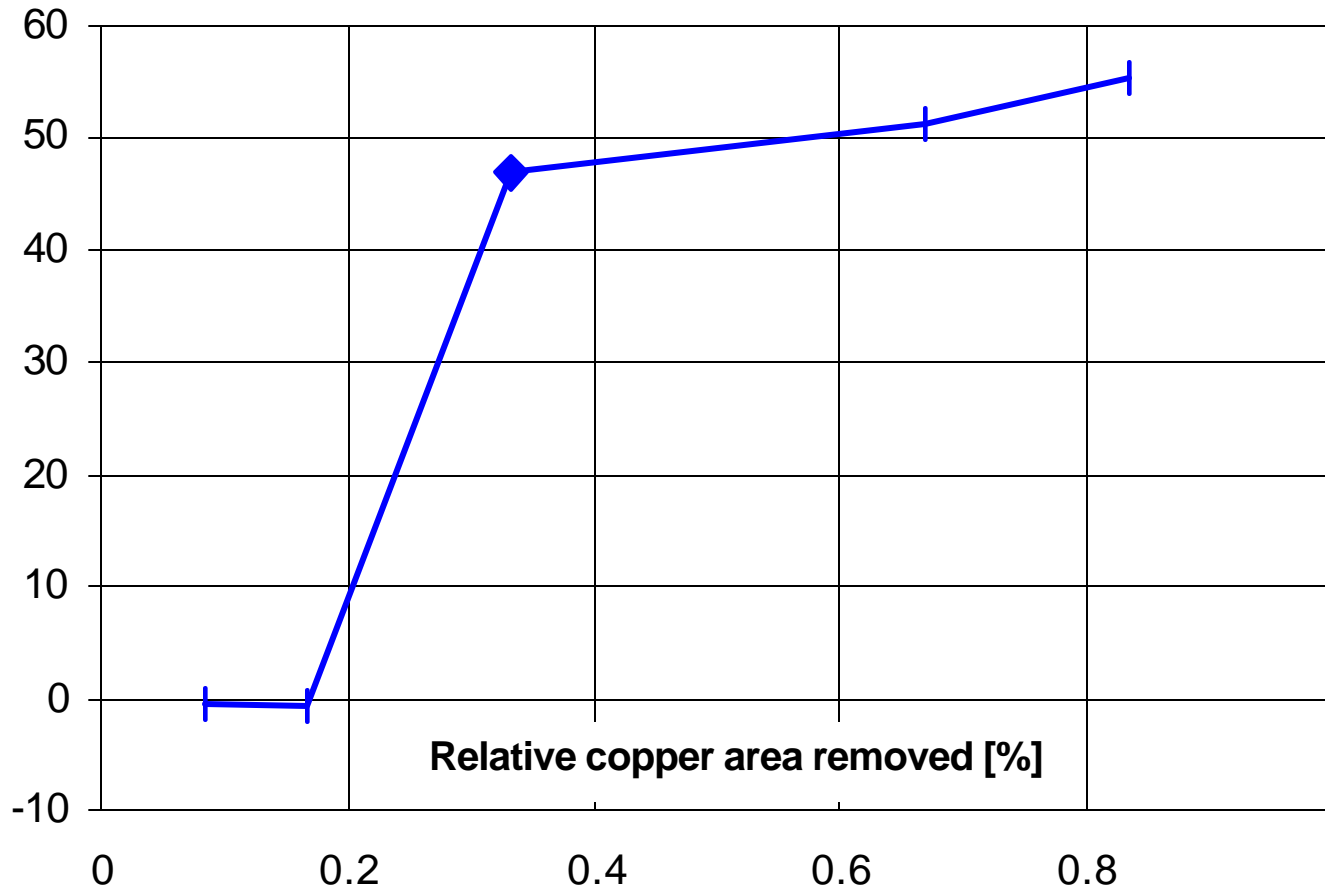
Cut from Side (2)

Impedance magnitude [ohm]



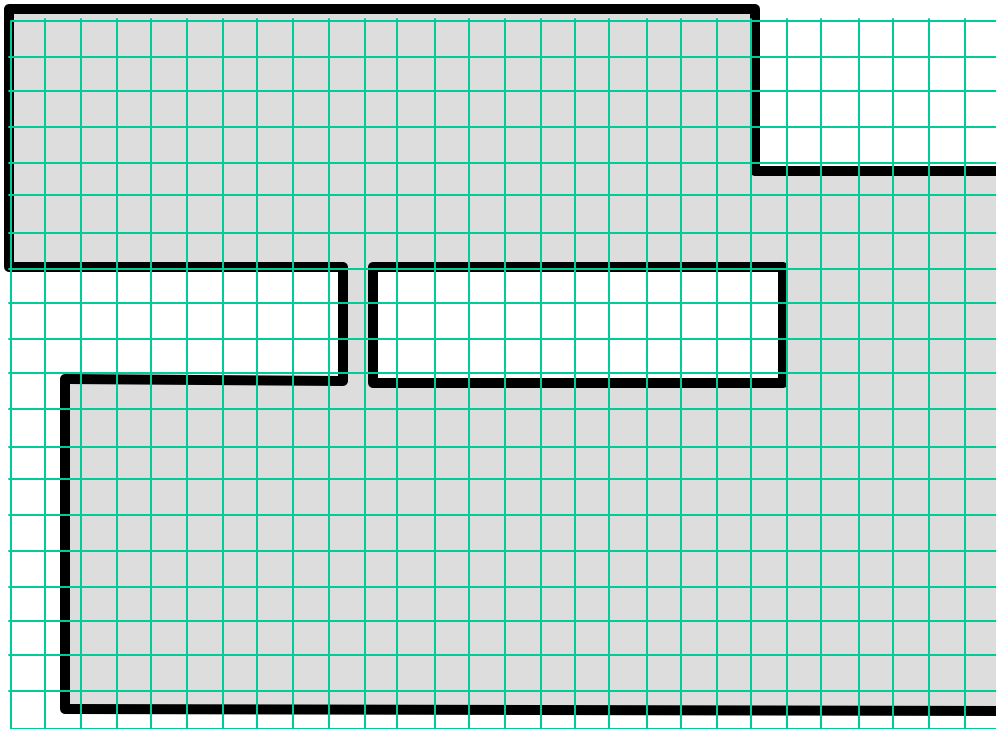
Cut from Side (3)

Percentage frequency change over percentage copper removed



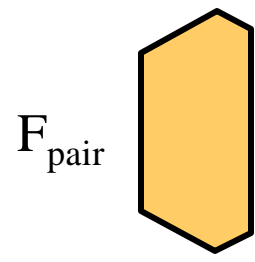
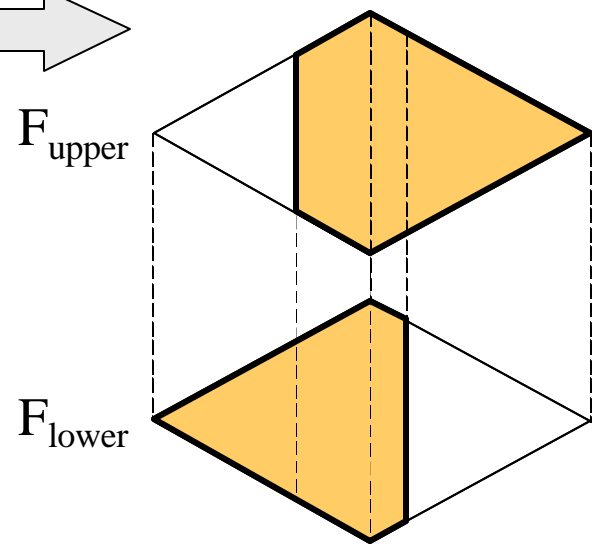
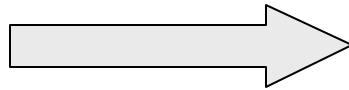
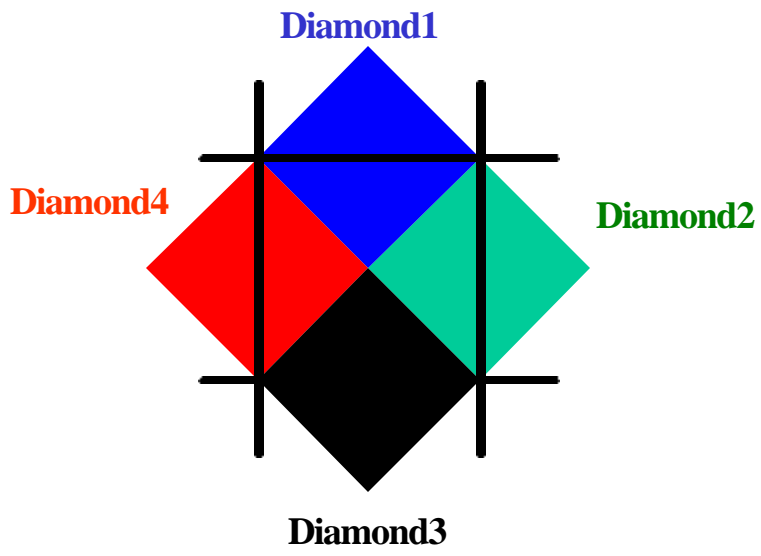
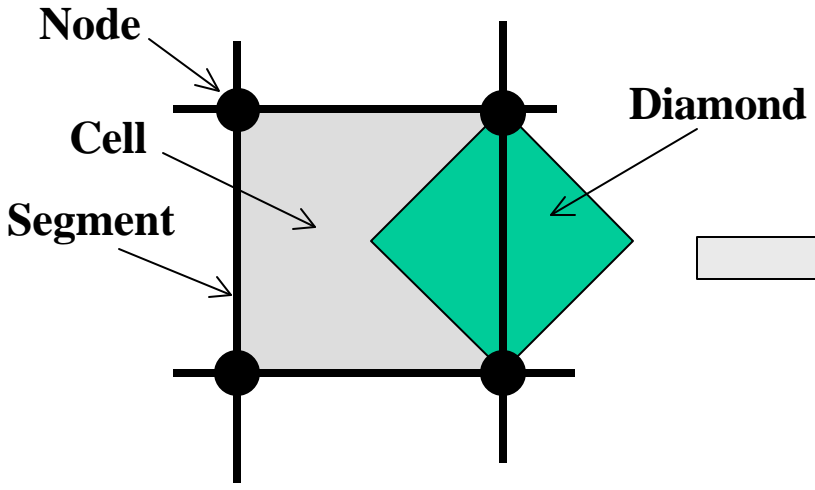
Frequency of first modal resonance peak

Limitations of Rectangular Uniform Grids

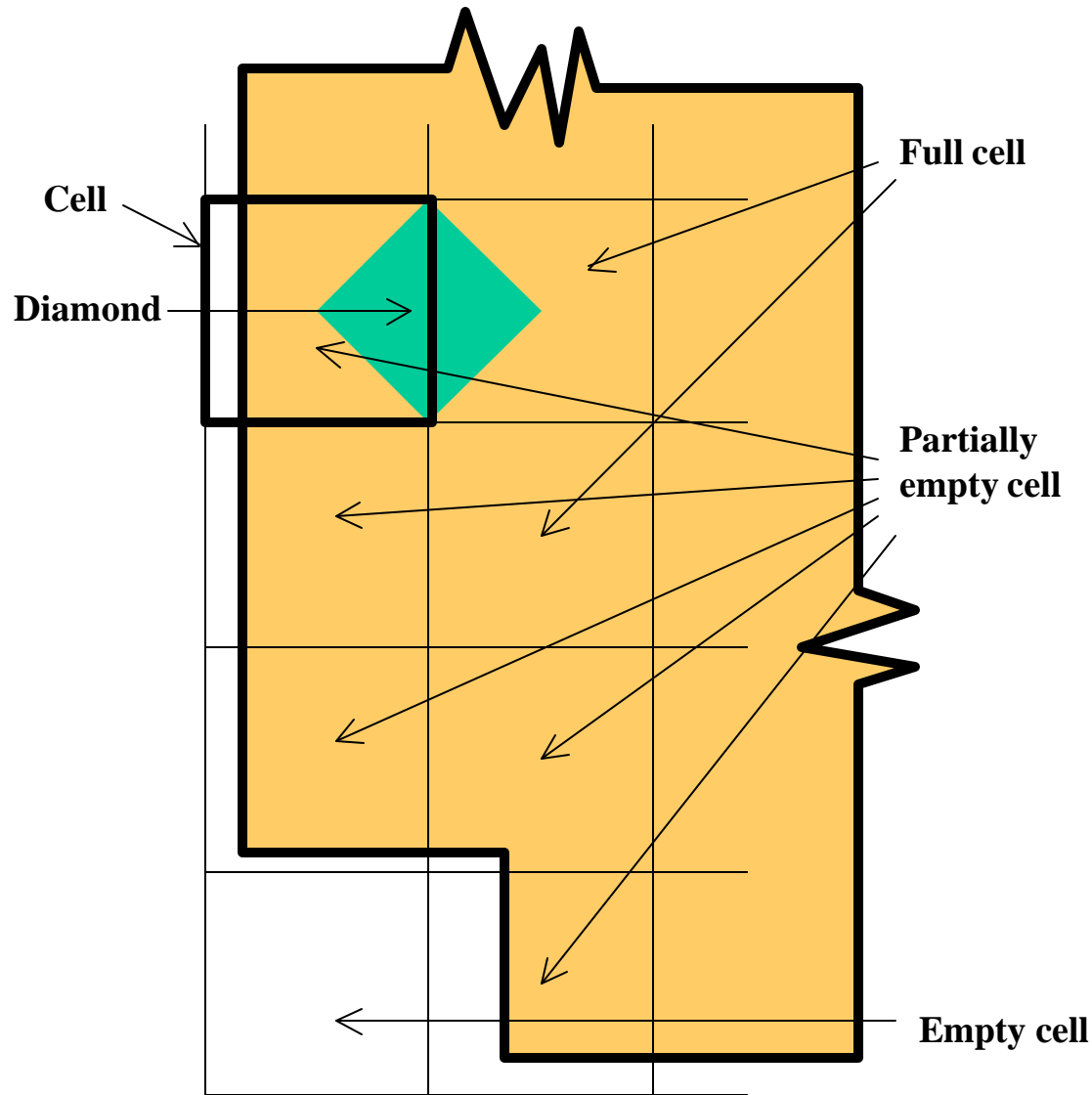


- Many cells may fall outside of shape
- SPICE run-time grows sharply with node numbers
 - Unnecessary nodes increase run time
 - Cant switch to fine mesh in sensitive areas
- Modal resonances may not be captured correctly

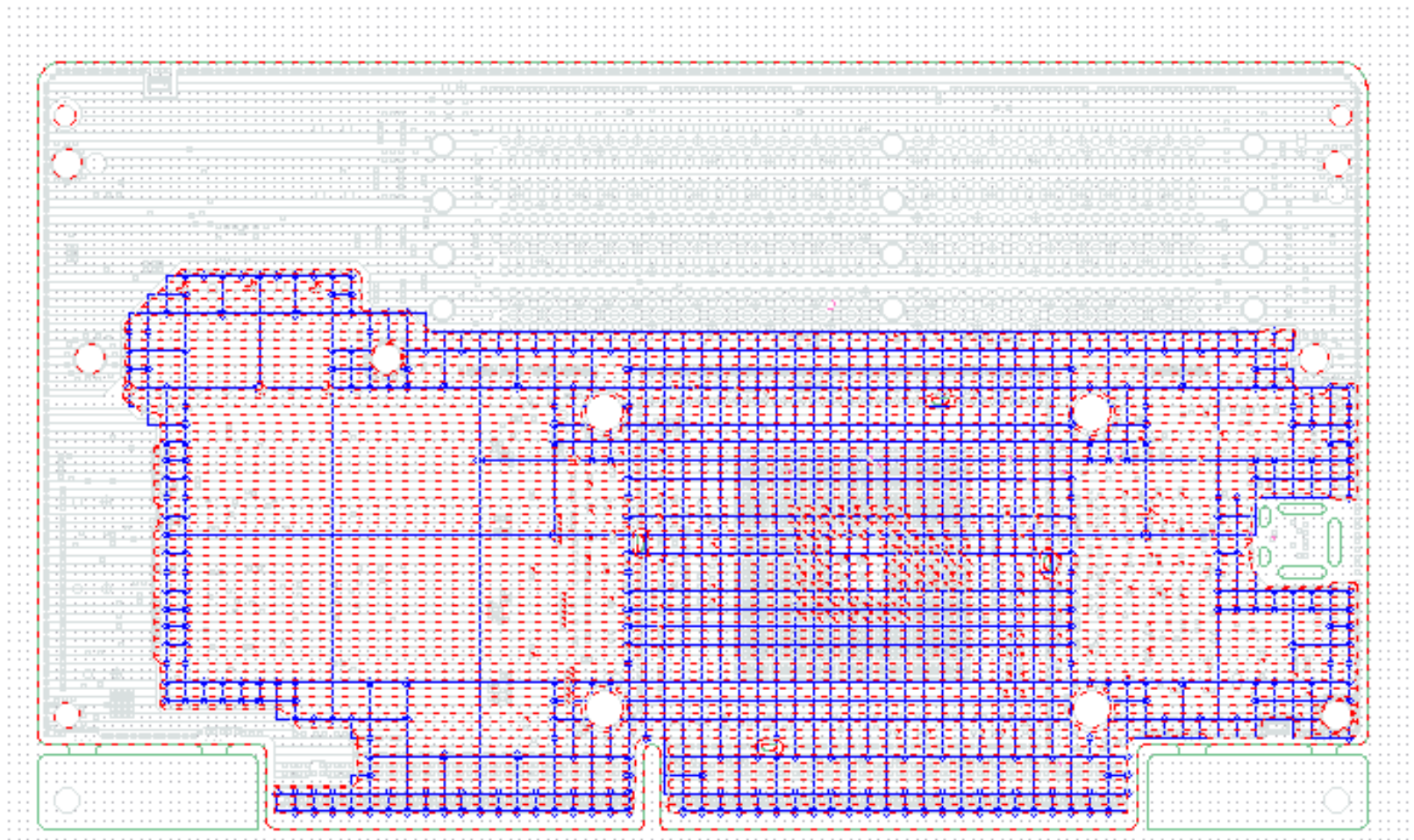
Cell and Diamond Definitions



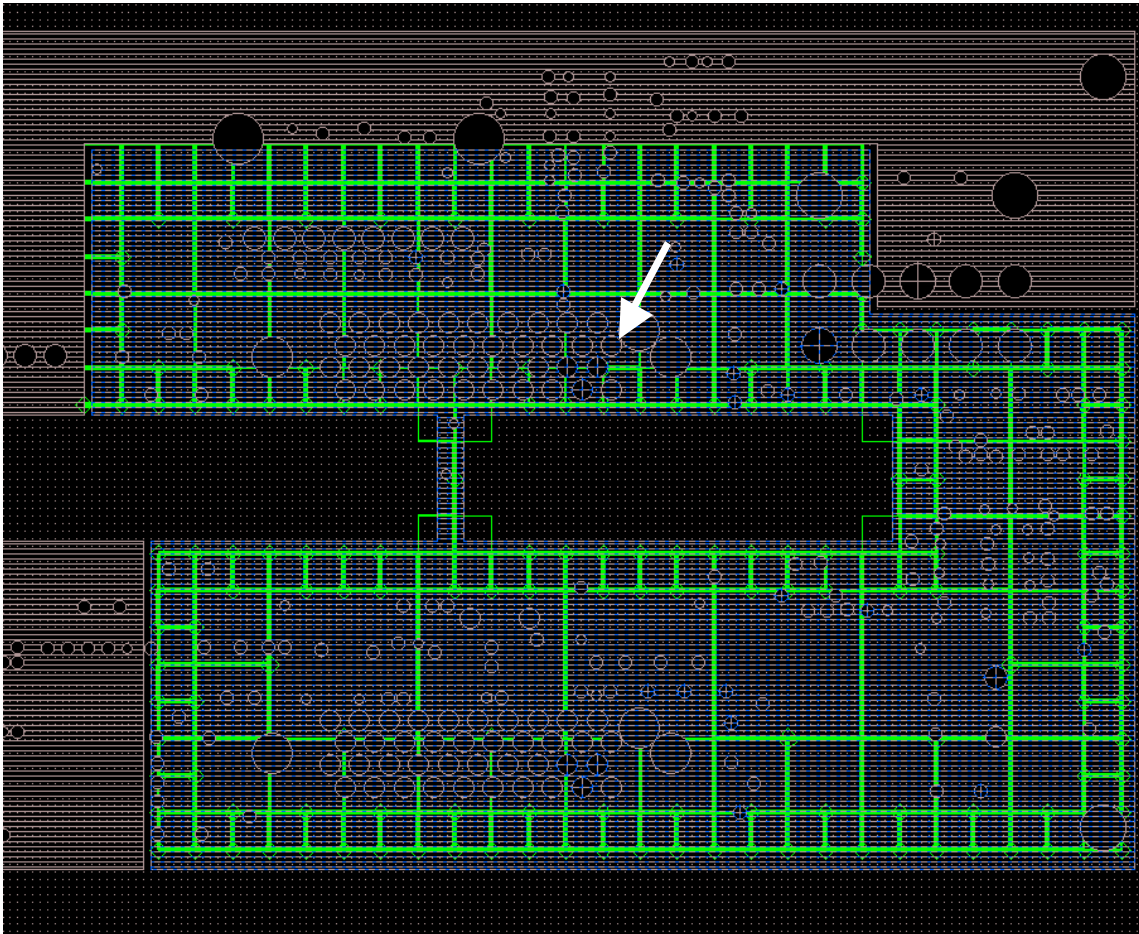
Definitions of Example Shape



Grid with Adaptive Sub Gridding



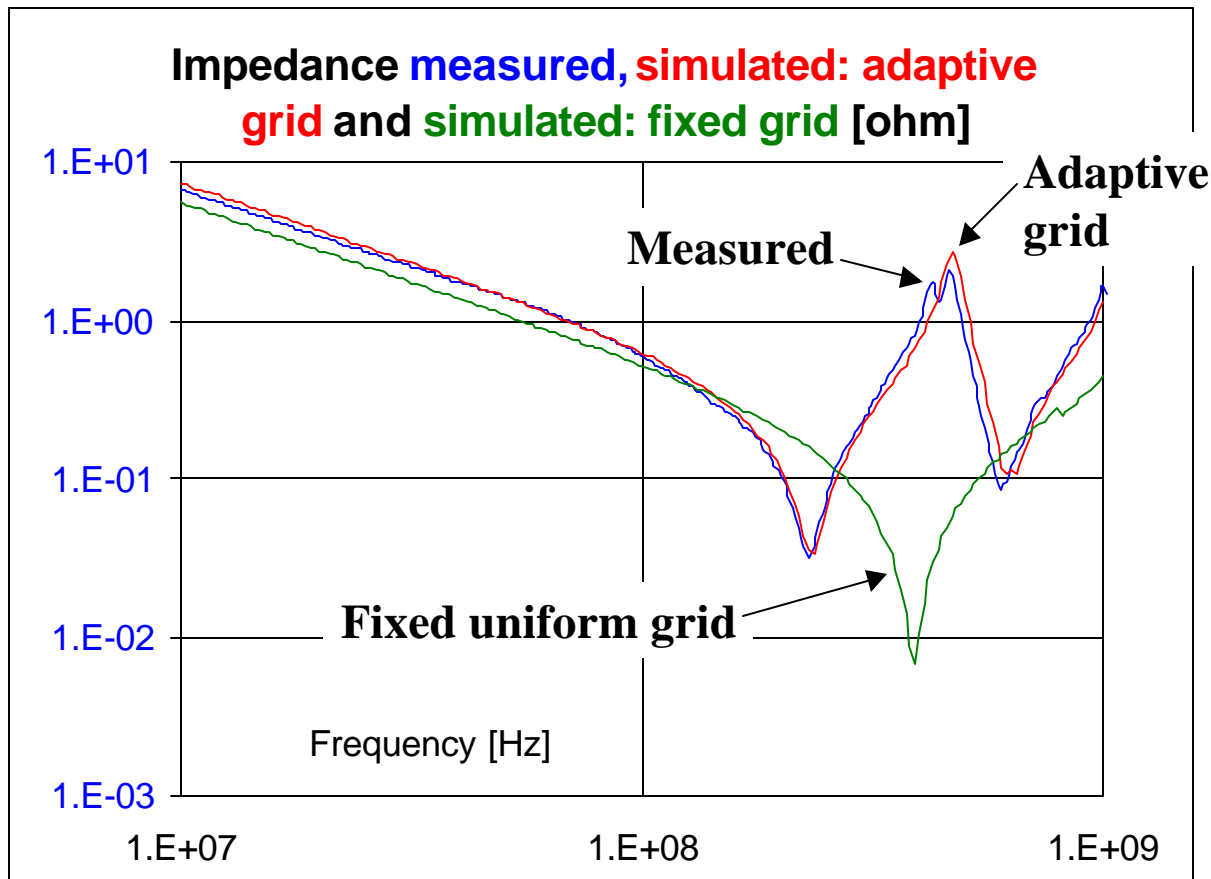
Correlation on Modal Resonances (1)



Example shape
from Slide 4:

- Irregular outline
- Cutouts

Correlation on Modal Resonances (2)



Self-impedance
at white arrow

Uniform grid:

- Overestimates static capacitance
- Overestimates resonance frequencies

Adaptive grid:

- Good correlation

Acknowledgement

Pre-processor SKILL script was written by Roger Cleghorn, Cadence

SPICE equivalent circuits were created by perl code, written by Ken Laird, North Eastern University

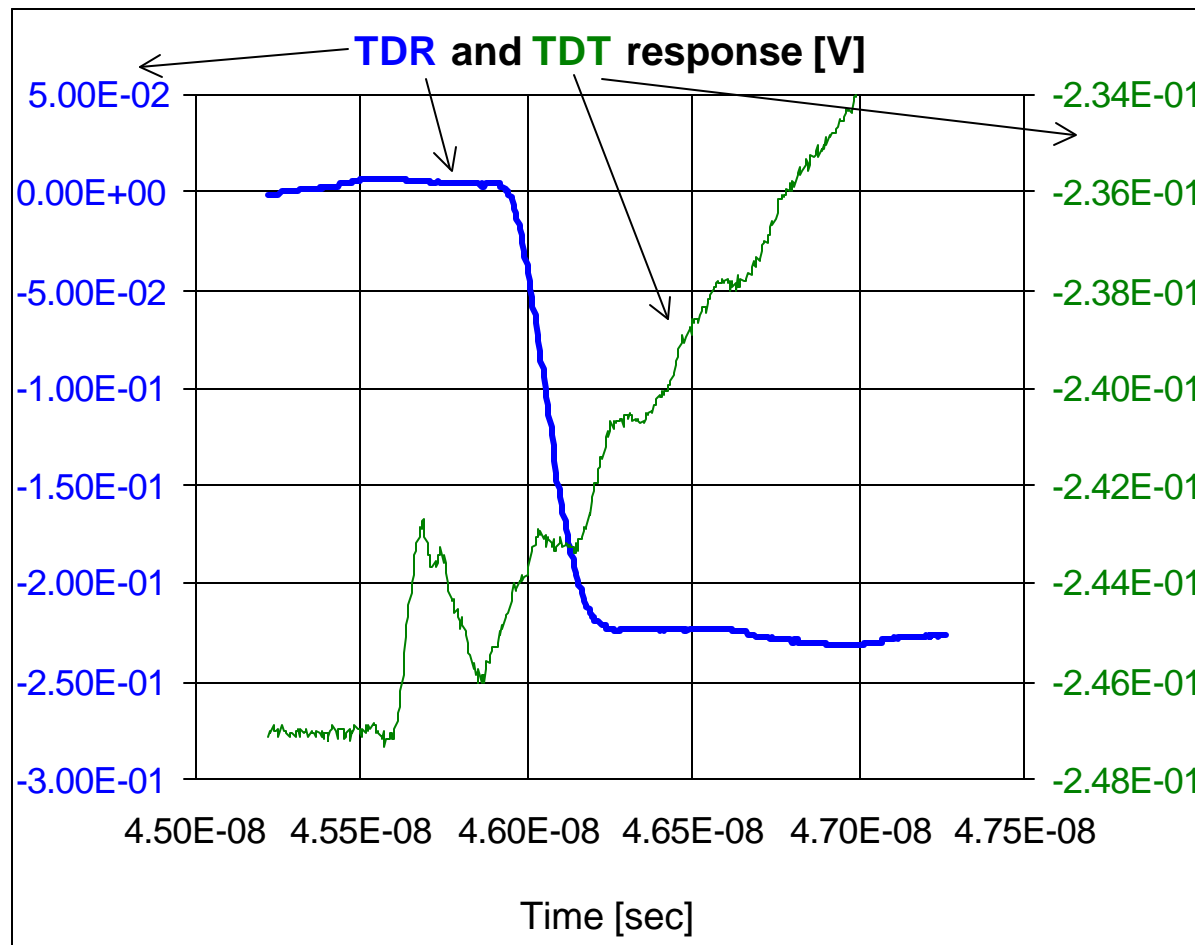
Further contributions and support:

- Hemant Shah (Cadence)
- Nick Laplaca (SUN)
- Deborah Foltz (SUN)
- Paul Baker (SUN)
- Paul Sorkin (SUN)

Conclusions

- Odd shapes, cutouts and perforations change
 - Static capacitance
 - Modal resonances
- Modal resonances do not scale with static capacitance
- Adaptive, non-uniform plane models can
 - Allow for finer mesh in critical areas
 - Capture modal resonances of odd shapes
 - Capture signatures of perforated planes
- Adaptive grid showed good hardware correlation

Correlation on Perforated Plane (1)



1.8"x1.6"x0.002"
Measured in the
middle, front/back
Via pair: 20mil drill,
50-mil center-to-
center

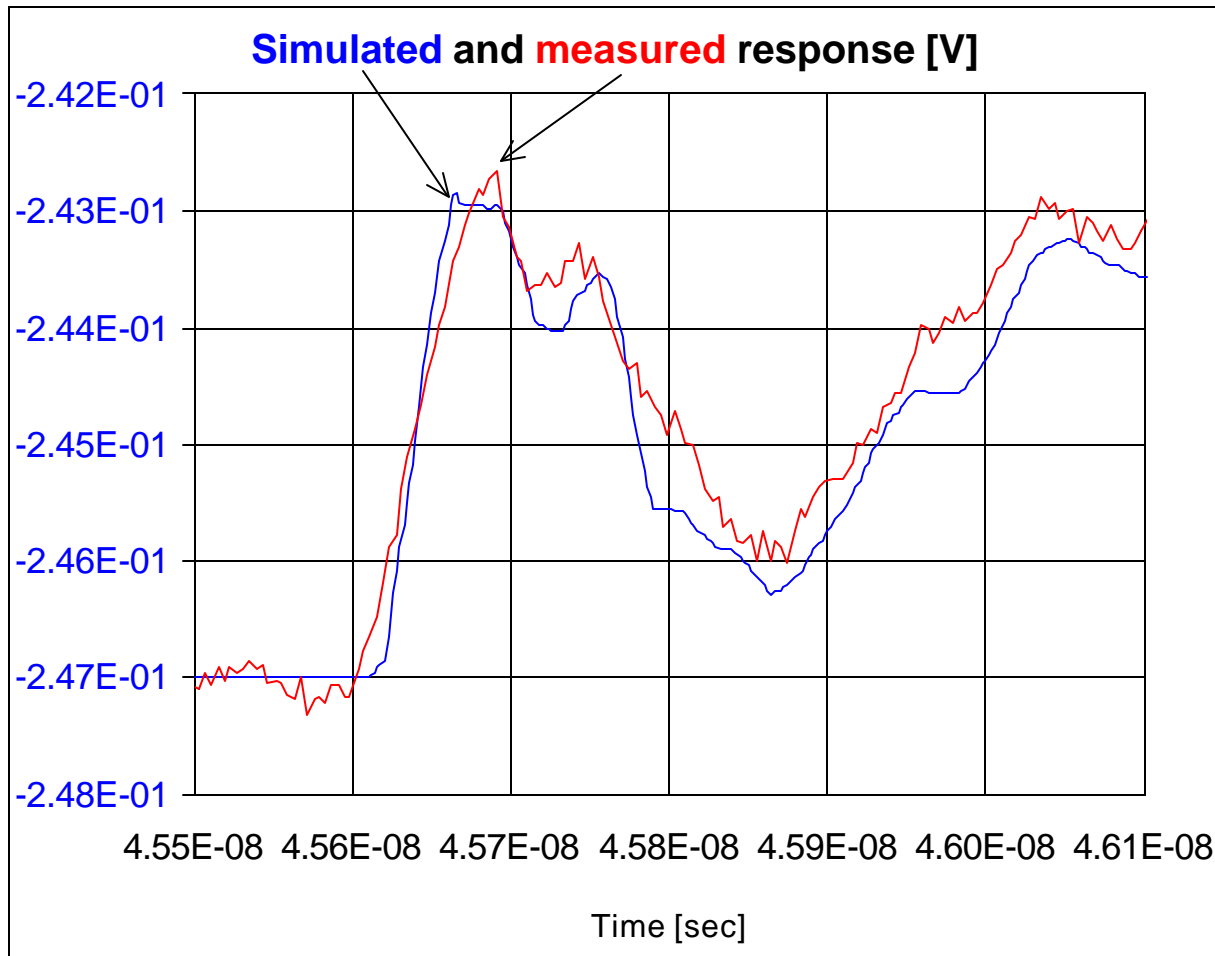
TDR source:

- 150psec
- 50 ohm

TDT input:

- 50 ohm

Correlation on Perforated Plane (2)



Adaptive grid captures accurately:

- Plane perforations
- Edge reflections